

Thin-gauge silicon steel strips and Applied products



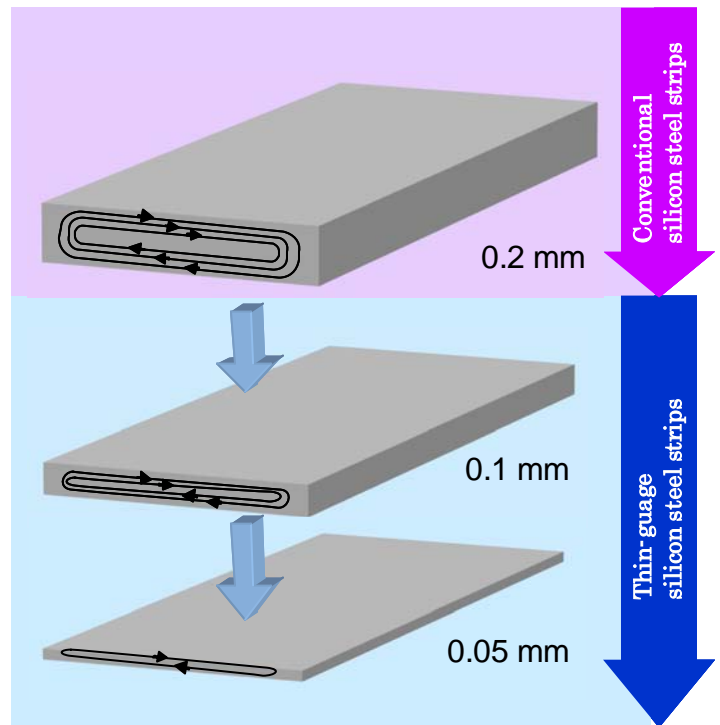
NIKKIN DENJI KOGYO Co., Ltd.

Thin-gauge silicon steel strips

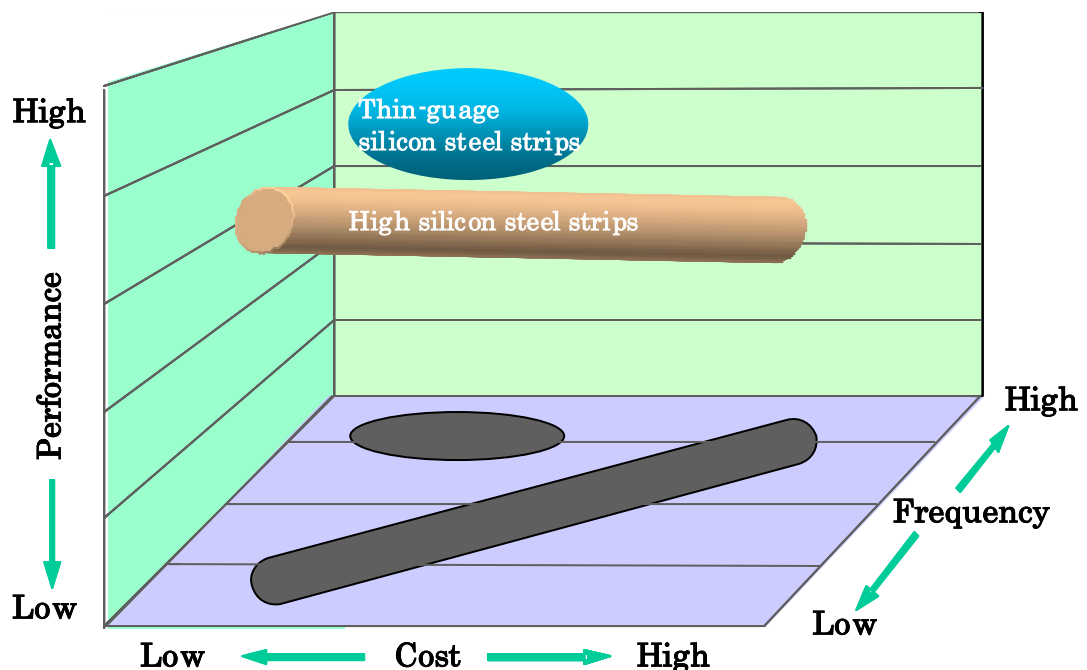
Conventional silicon steels are widely used for electrical power apparatus, electrical components in industrial products and home electronics. However, most silicon steel strips are more than 0.2mm in thickness, and applied only to apparatus operated at industrial frequencies.

On the other hand, thin-gauge silicon steel strips have advantage for use at higher frequencies. The thickness of our silicon steel strips have been reduced to the world's thinnest level so that the core loss caused by eddy currents is compressed to the lowest level and combined with our insulation coating technology, the lamination factor has been improved. Our thin-gauge silicon steel strips assist saving energy and down-sizing high-frequency reactors, transformers, and motors.

Our thin-gauge silicon steel strips allow superior cost saving as well as performance at high frequencies.



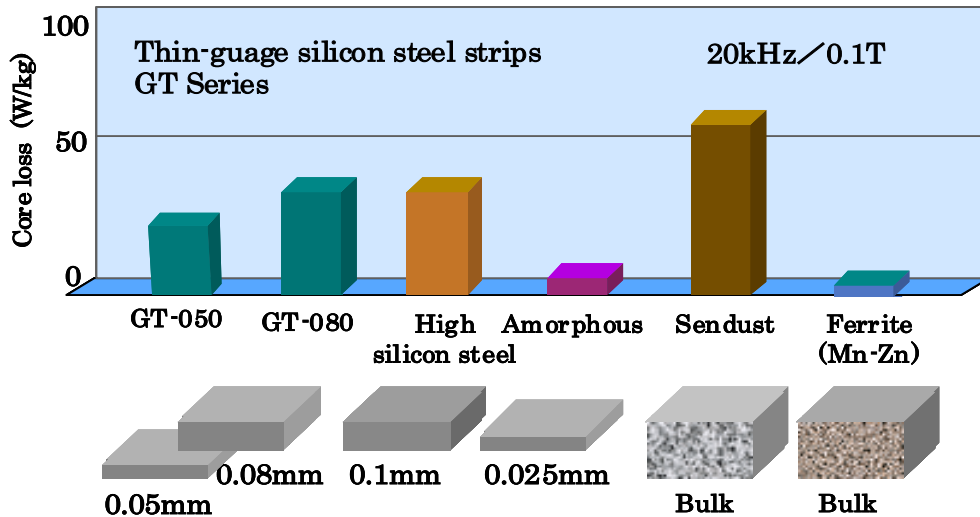
Very low core loss can be achieved by using thin-gauge strips due to its small eddy currents.



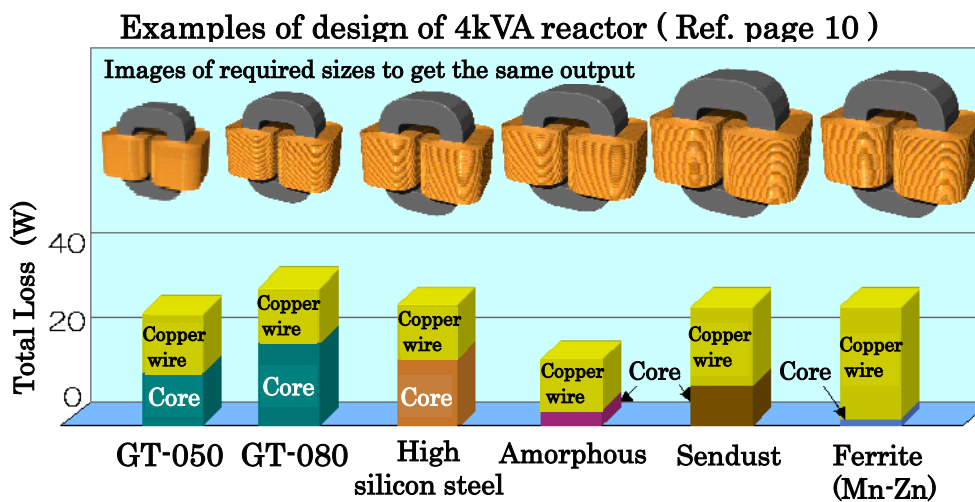
◆ Thin-gauge silicon steel strips provide superior cost performance at high frequencies.

Cost performances of thin-gauge silicon steel strips

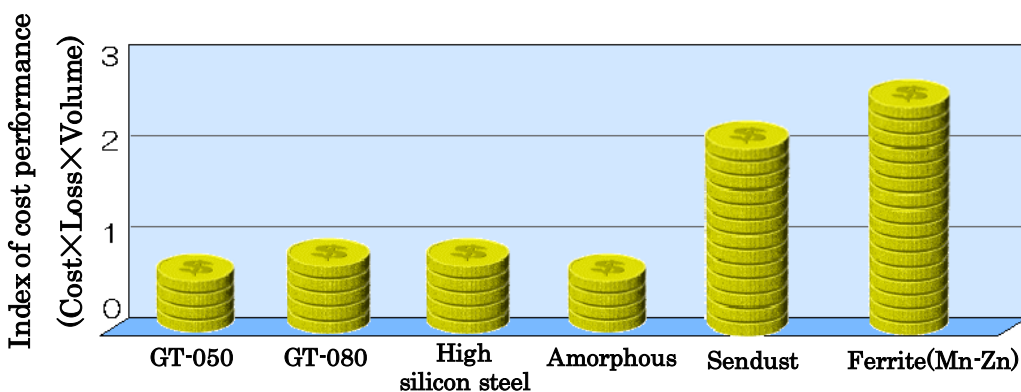
Have materials been chosen for their characteristics ?



Amorphous and ferrite exhibit excellent performance in a evaluation of the core loss.



Evaluation of performance will change according to the total loss including losses from the size and copper wires.



Additionally, considering cost performance, the advantages of thin-gauge silicon steel strips is apparent.

- ◆ Thin-gauge silicon steel strips demonstrate their true abilities only after application.
- ◆ Thin-gauge silicon steel strips contribute to down sizing , saving energy and lower costs.

Types and applications of thin-gauge silicon steel strips

Table 1 Types of thin-gauge silicon steel strips

| Classification | Grade | Thickness | Characteristics |
|---|---------|-----------|--|
| GT series Oriented thin-gauge silicon steel strips | GT-100 | 0.10mm | * Similar oriented magnetic properties relative to the rolling direction * Very low core loss at high frequencies and high saturation flux density * Most suitable for reactors, transformers, and shields |
| | ※GT-080 | 0.08mm | |
| | GT-050 | 0.05mm | |
| | ※GT-040 | 0.04mm | |
| ST series Non-oriented thin-gauge silicon steel strips | ST-150 | 0.15mm | * The same as magnetic properties of GT series * No orientation in magnetic properties * Most suitable for motors, shields and also for high frequency reactors |
| | ST-100 | 0.10mm | |
| | ST-050 | 0.05mm | |

Notes) Grade(※) shows newly developed products.

Thin-gauge silicon steel strips

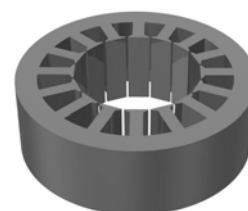


Applications of the GT series



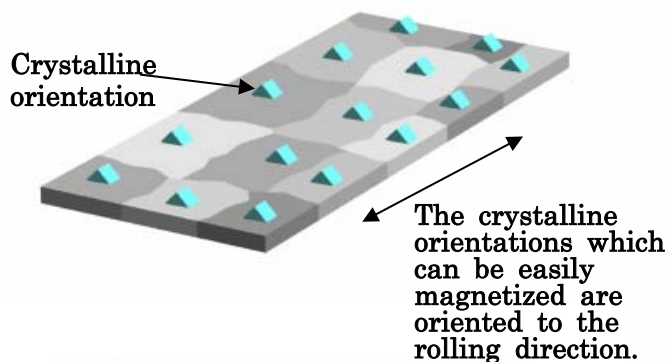
High-frequency reactors

Applications of the ST series



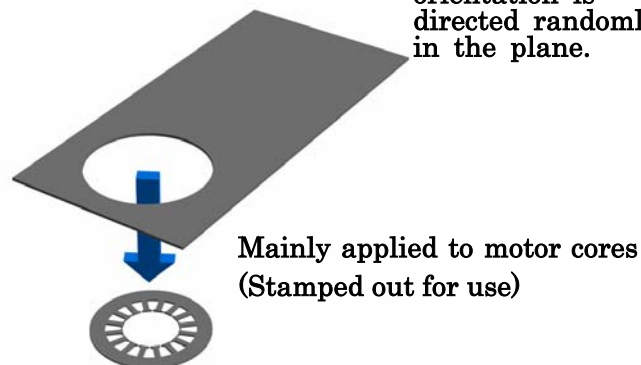
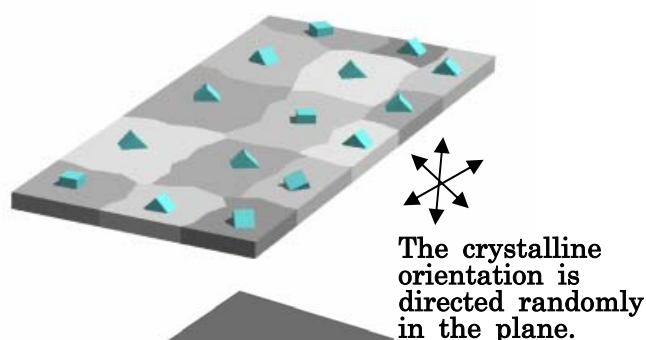
Motor cores

◆ Oriented thin-gauge silicon steel strips

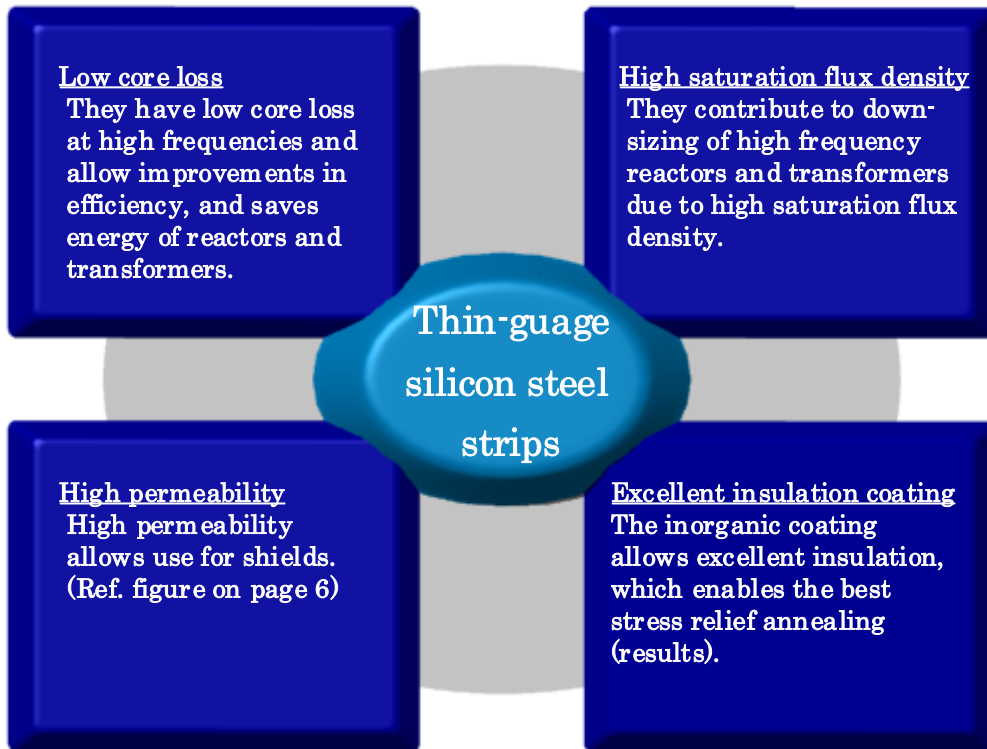


Mainly applied to wound cores (Wound for use)

◆ Non-oriented thin-gauge silicon steel strip



Characteristics of thin-gauge silicon steel strips

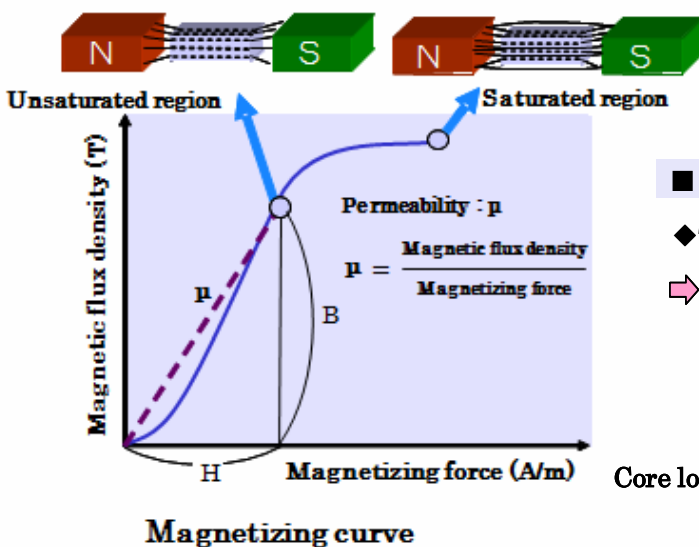


<Reference > Required properties for magnetic materials

- High flux density, High permeability

◆ Magnetic force becomes stronger as the magnetic flux density B and the permeability μ increases.

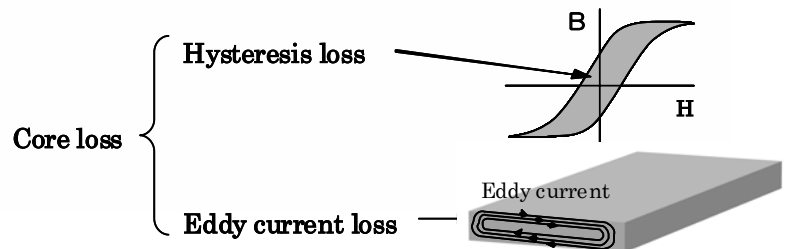
⇒ Down-sizing and weight-saving becomes possible.



- Low core loss

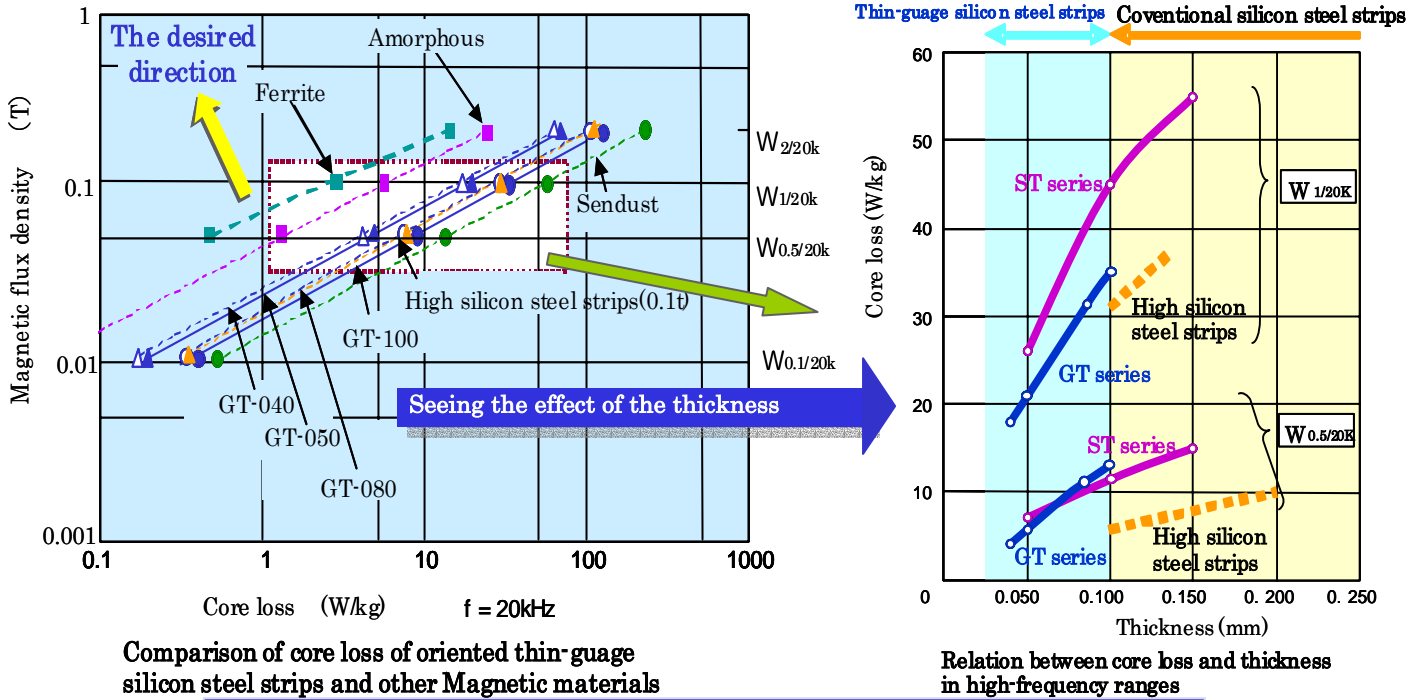
◆ The lower the core loss, the smaller the energy loss.

⇒ Energy saving and high efficiency are achieved.



The joule heat caused by eddy currents increases the energy loss.

Core loss of thin gauge silicon steel strips at high frequencies

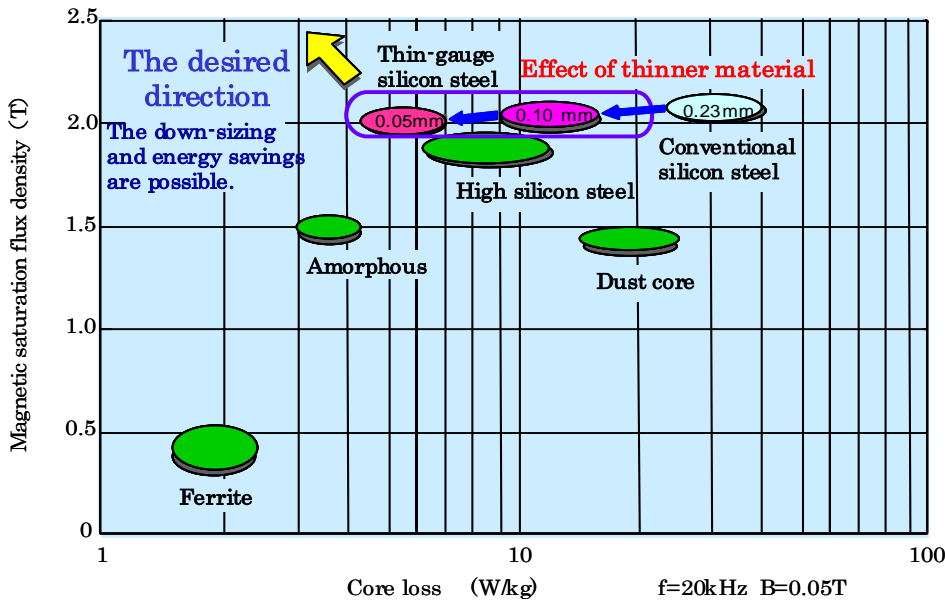


Comparison of core loss of oriented thin-gauge silicon steel strips and other Magnetic materials

Relation between core loss and thickness in high-frequency ranges

The thickness significantly effects core loss, therefore, allowing thin with very low core loss at high frequencies to contribute to higher efficiency and saving energy.

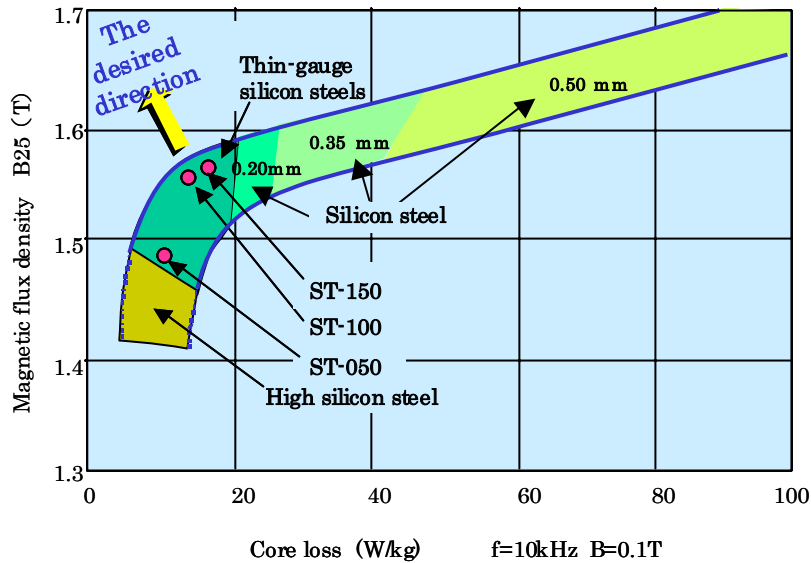
Magnetic saturation flux density of oriented thin gauge silicon steel strips



Comparison of magnetic properties of oriented thin-gauge silicon steel strips and other magnetic materials

Thin-gauge silicon steel strips have high saturation flux density which contributes to the downsizing.

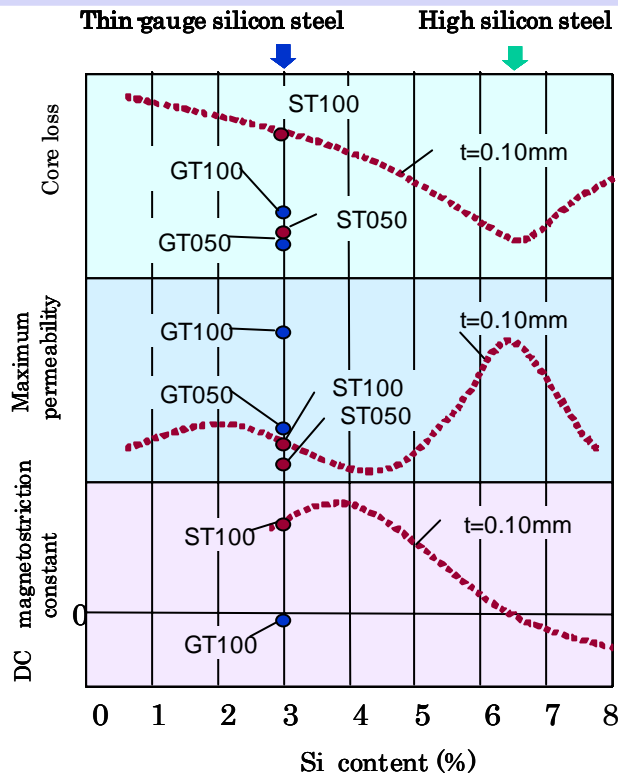
Magnetic flux density of non-oriented thin-gauge silicon steel strips



Comparison of core loss of non-oriented thin-gauge silicon steel strips with other non-oriented silicon steel strips

Non-oriented thin-gauge silicon steel strips is the ideal material due to its low core loss and high saturation flux density.

Comparison of magnetic properties of silicon steel



Magnetic properties of silicon steels

The most suitable thin-gauge silicon steel strips can be selected according to the required magnetic properties.



The design of applied products

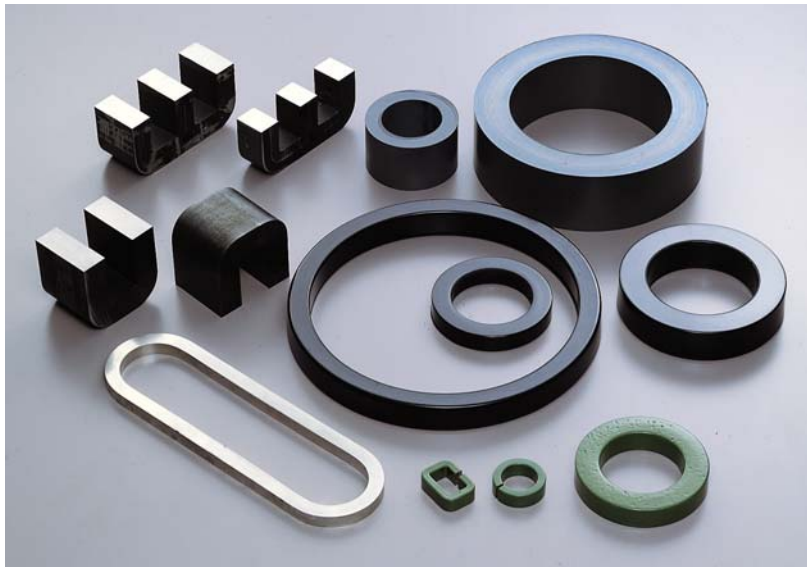
We sell thin-gauge silicon steel strips as well as designing, manufacturing, and sales of wound cores and applied products in which thin-gauge silicon steel strips are used.

Based on our wealth of technical experience, we can design and manufacture the products to meet your demands. We offer wound cores in small lots which exhibit excellent cost performances. Using our wound cores is less costly than stamped cores since die assembly is unnecessary.

We assist customers in selecting suitable cores by using our wealth of technical experience.

Examples of application

We manufacture various wound cores and reactors.



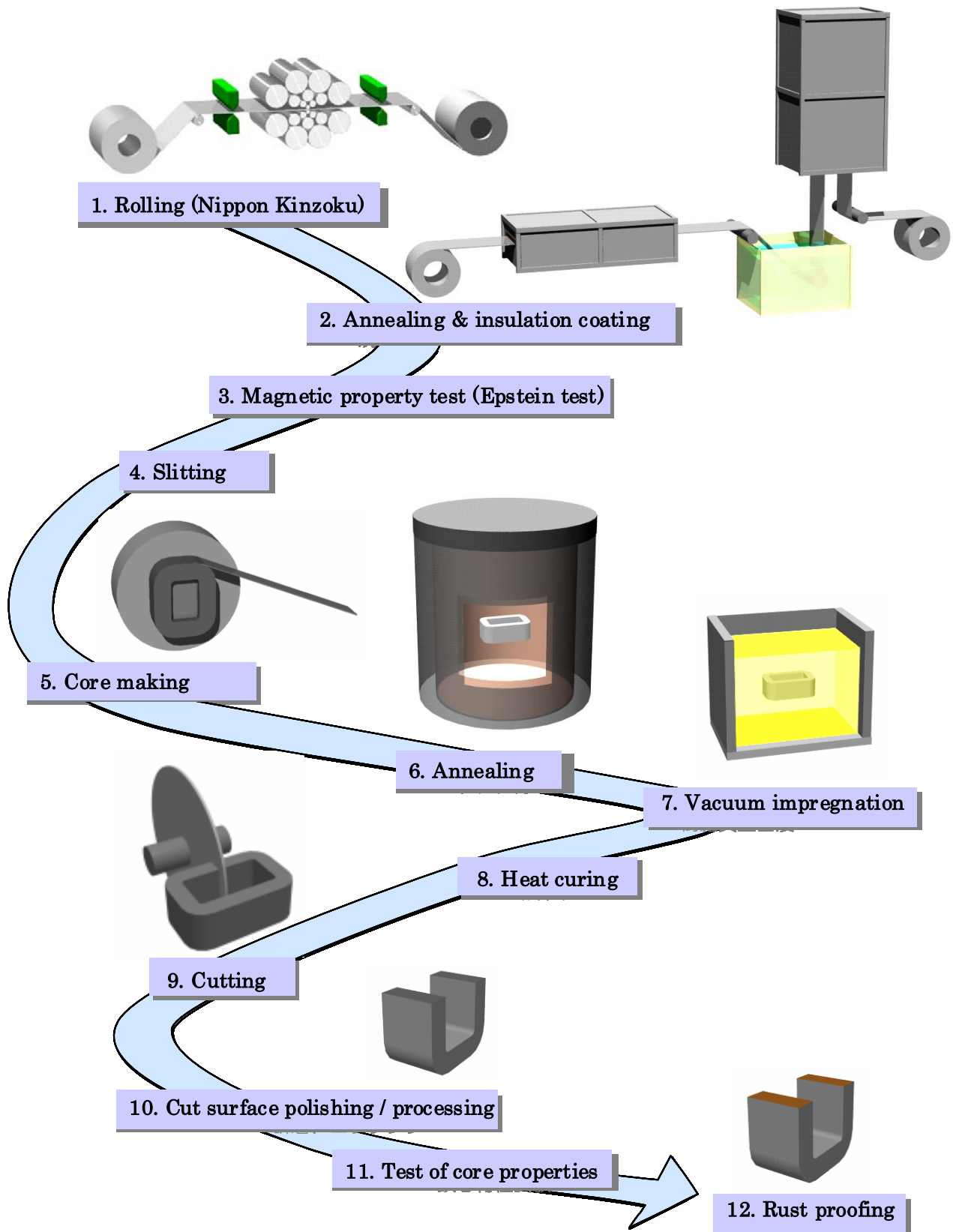
Wound cores



Applied products
(Electronic parts)

Manufacturing process of applied products

From rolling to assembly, we manufacture thin-gauge silicon steel strips and applied products under strict quality control.

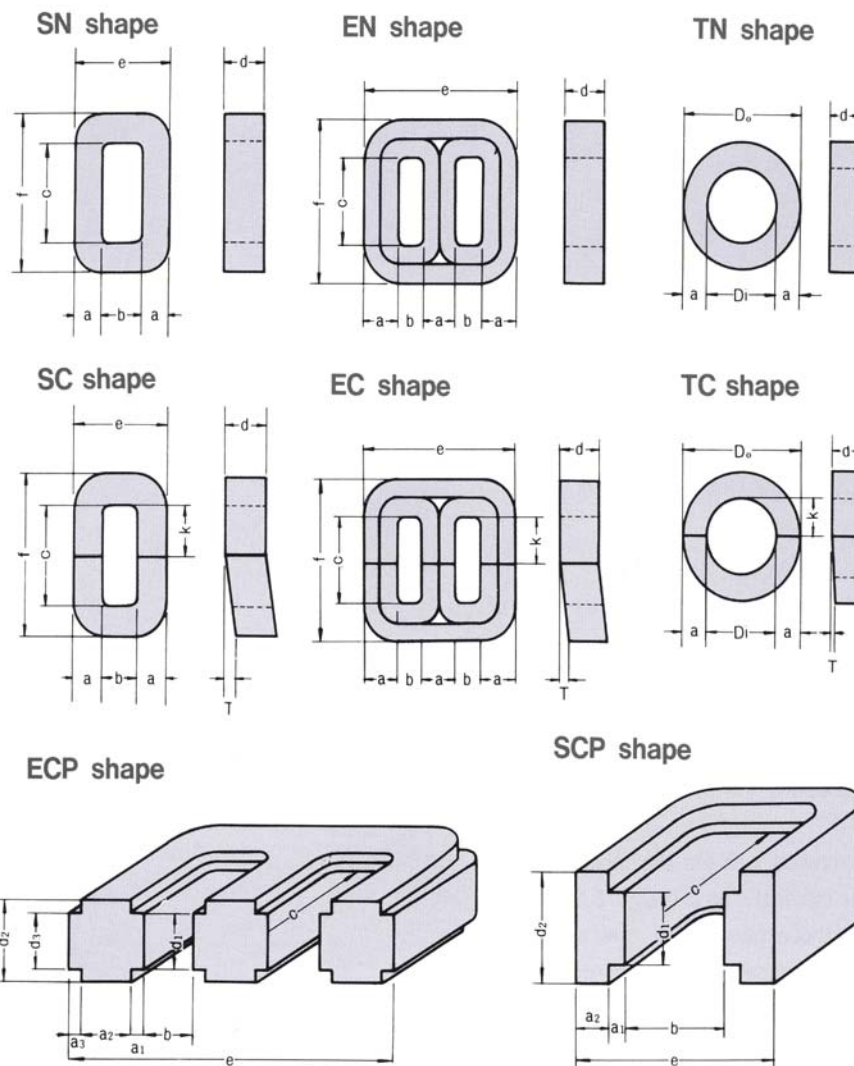
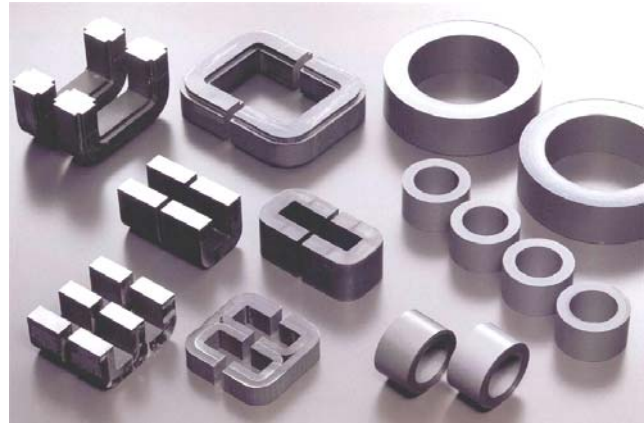


Standard cores : CS series, SC series, EC series

Wound cores are available to meet customers requirements.
Please specify the following.

Table 2 Dimensional notations

| Shape | Notations |
|-------|---|
| SN | SN $a \times b \times c \times d$ ($\times e \times f - R$) |
| EN | EN $a \times b \times c \times d$ ($\times e \times f - R$) |
| TN | TN $a \times d \times D_i$ ($\times D_o$) |
| SC | SC $a \times b \times c \times d$ ($\times e \times f - R$) |
| EC | EC $a \times b \times c \times d$ ($\times e \times f - R$) |
| TC | TC $a \times d \times D_i$ ($\times D_o$) |
| ECP | ECP $a_1 \times b \times c \times d_1$ ($\times e \times f - R$) $a_2 \times b \times c \times d_2$ $a_3 \quad d_3$ |
| SCP | SCP $a_1 \times b \times c \times d_1$ ($\times e \times f - R$) $a_2 \quad d_2$ |



Design examples

The following is the example of a reactor for 4kVA photovoltaics generation. We can design the optimal reactor, by the specifications of inductance, rated current, carrier frequency, carrier current, etc.

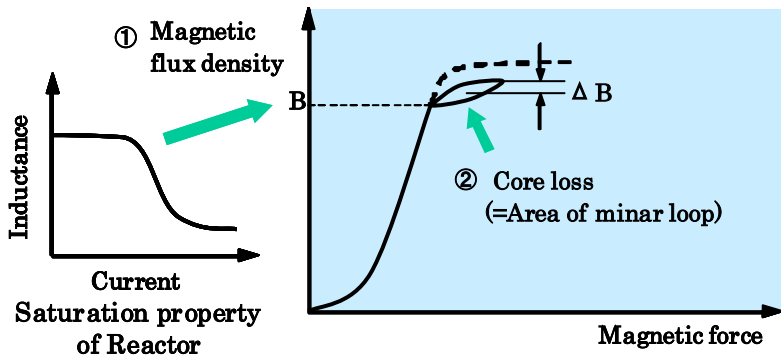
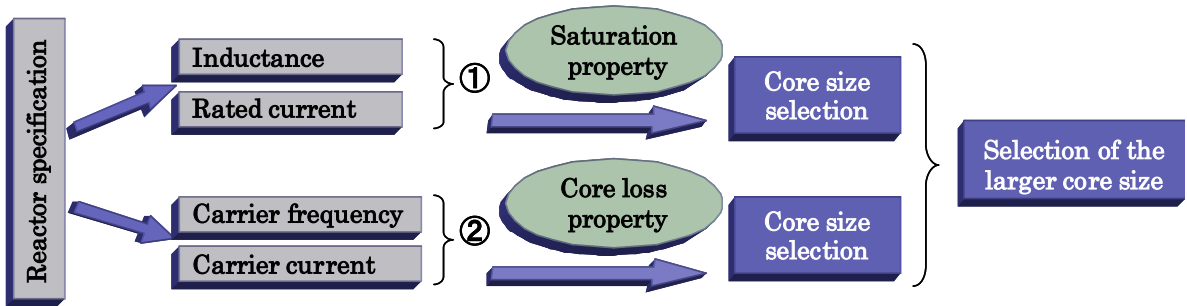


Table 3 Comparison of designs of reactors between various magnetic materials

| Materials | | GT-100 | GT-080 | GT-050 | GT-040 | High silicon steel 0.1t | Amorphous | Sendust | Ferrite Mn-Zn |
|--------------------------|-------------------------------|------------|--------|--------|--------|-------------------------|-----------|---------|---------------|
| | | Parameters | | | | | | | |
| Electrical specification | Inductance(μH) | 1000 | ← | ← | ← | ← | ← | ← | ← |
| | Rated current (A) | 25 | ← | ← | ← | ← | ← | ← | ← |
| | Frequency(kHz) | 20 | ← | ← | ← | ← | ← | ← | ← |
| | Carrier current(Ap-p) | 5 | ← | ← | ← | ← | ← | ← | ← |
| | Inductance(μH)at50A | ≥ 600 | ← | ← | ← | ← | ← | ← | ← |
| | Temperature rise(K) | ≤ 70 | ← | ← | ← | ← | ← | ← | ← |
| Core | B(T) | 0.90 | 1.03 | 1.06 | 1.06 | 0.87 | 0.91 | 0.39 | 0.46 |
| | Core loss(W) | 19.1 | 14.4 | 11.5 | 9.2 | 14.8 | 3.2 | 5.7 | 1.1 |
| | Mass(kg) | 1.27 | 1.11 | 0.96 | 0.92 | 1.23 | 1.27 | 2.27 | 1.10 |
| | Ratio of cost *1 | 1.00 | 0.92 | 0.97 | 0.97 | 1.03 | 1.16 | 1.19 | 1.20 |
| Coil | DC resistance(mΩ) | 20.1 | 18.9 | 20.3 | 20.7 | 20.1 | 19.4 | 31.5 | 38.4 |
| | Copper loss(W) | 12.6 | 11.8 | 12.7 | 13.0 | 12.6 | 12.2 | 19.7 | 24.2 |
| | Mass(kg) | 0.60 | 0.57 | 0.61 | 0.62 | 0.60 | 0.58 | 1.13 | 1.63 |
| | Ratio of cost *1 | 1.00 | 0.95 | 1.02 | 1.03 | 1.00 | 0.97 | 1.88 | 2.72 |
| Reactor | Total mass(kg) | 1.87 | 1.68 | 1.57 | 1.54 | 1.83 | 1.85 | 3.40 | 2.73 |
| | Ratio of Loss(%) *2 | 0.79 | 0.66 | 0.61 | 0.56 | 0.69 | 0.39 | 0.64 | 0.63 |
| | ①Ratio of volume *1 | 1.00 | 0.92 | 0.87 | 0.83 | 1.00 | 1.09 | 2.00 | 1.99 |
| | ②Ratio of loss *1 | 1.00 | 0.83 | 0.77 | 0.70 | 0.86 | 0.49 | 0.80 | 0.80 |
| | ③Ratio of cost *1 | 1.00 | 0.93 | 0.98 | 0.98 | 1.02 | 1.11 | 1.36 | 1.57 |
| | ④Index of cost performance *3 | 1.00 | 0.71 | 0.65 | 0.57 | 0.88 | 0.59 | 2.18 | 2.49 |

*1 Values are calculated on the condition that values of GT-100 are set at 1.00.
 *2 Ratio of loss is the ratio of total loss (core loss plus copper loss) to capacity (4kVA).
 *3 Index of cost performance is calculated as ① × ② × ③. (The smaller number, better cost performance)

Dimension of thin-gauge silicon steel strips

Table 4 Dimension

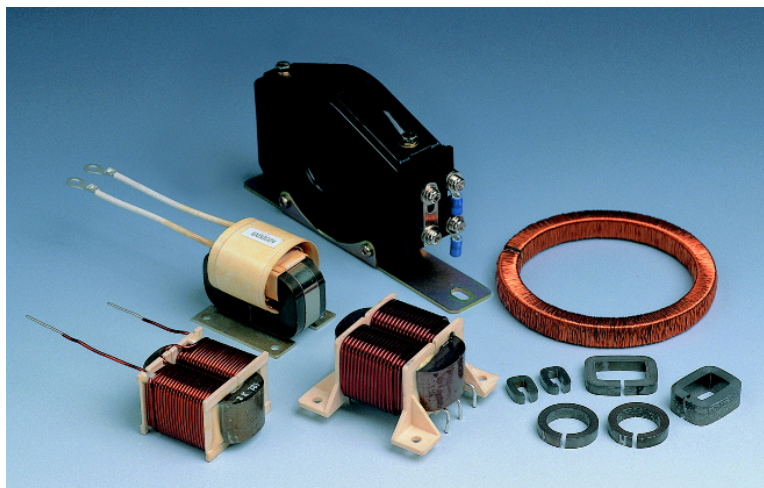
| Grade | Thickness | | Cross-directional thickness deviation (mm) | Width | | Coil inner diameter (mm) |
|--------|----------------|------------------|--|----------------|----------------|--------------------------|
| | Dimension (mm) | Tolerance (mm) | | Dimension (mm) | Tolerance (mm) | |
| GT-100 | 0.10 | +0.010 -0.015 | 0.010 | MAX 300 | ±0.4 | 250 |
| GT-050 | 0.05 | +0.008 -0.010 | 0.010 | MAX 300 | ±0.4 | 250 |
| ST-150 | 0.15 | ±0.020 | 0.020 | MAX 300 | ±0.4 | 250 |
| ST-100 | 0.10 | +0.010 -0.015 | 0.010 | MAX 300 | ±0.4 | 250 |
| ST-050 | 0.05 | +0.008 -0.010 | 0.010 | MAX 300 | ±0.4 | 250 |

Standard values of thin-gauge silicon steel strips

Table 5 Standard values of thin-gauge silicon steel strips

| Grade | Core loss(W/kg) | | | Magnetic flux density(T) | |
|--------|---------------------|---------------------|----------------------|--------------------------|-----------------|
| | W _{10/400} | W _{15/400} | W _{10/1000} | B ₈ | B ₅₀ |
| GT-100 | — | ≤15 | — | ≥1.7 | — |
| GT-050 | — | — | ≤24 | ≥1.6 | — |
| ST-150 | ≤14 | — | — | — | ≥1.6 |
| ST-100 | ≤13 | — | — | — | ≥1.6 |
| ST-050 | — | — | — | — | ≥1.5 |

- Notes) 1. For GT series, the specimens are taken from the strips parallel to the rolling direction. The measurements are in accordance with JIS C 2550 after stress relief annealing.
2. For ST series, the specimens are taken from the strips in both directions of parallel and transverse to the rolling direction. The measurements are in accordance with JIS C 2550.
3. W_{10/400}, W_{15/400} and W_{10/1000} show core losses at magnetic flux densities 1.0T(10kG), 1.5T(15kG) and 1.0T(10kG), and frequencies 400Hz, 400Hz and 1000Hz, respectively.
4. B₈ and B₅₀ show magnetic flux densities at magnetic force 800A/m and 5000A/m.



Magnetic properties of thin-gauge silicon steel strips

Table 6 Core loss properties

| Grade | Core loss (W/kg) | | | | | | | |
|--------|--------------------|---------------------|---------------------|----------------------|---------------------|---------------------|----------------------|------------------------|
| | W _{15/50} | W _{15/100} | W _{10/400} | W _{10/1000} | W _{5/2000} | W _{2/5000} | W _{1/10000} | W _{0.5/20000} |
| GT-100 | 1.2 | 3.0 | 6.1 | 21.3 | 18.0 | 15.2 | 10.4 | 13.0 |
| GT-050 | 1.7 | 5.0 | 7.3 | 17.0 | 13.0 | 10.2 | 7.1 | 5.3 |
| ST-150 | 2.3 | — | 11.6 | 39.4 | 30.0 | 21.5 | 17.2 | 14.2 |
| ST-100 | 2.7 | — | 11.0 | 34.1 | 25.3 | 17.0 | 12.9 | 10.2 |
| ST-050 | 6.1 | — | 25.4 | 65.8 | 40.8 | 21.4 | 11.6 | 6.7 |

Table 7 Permeability and magnetic flux density properties

| Grade | Alternating permeability × 10 ⁻³ (H/m) | | | | | Magnetic flux density(T) | | |
|--------|---|----------------------|---------------------|----------------------|------------------------|--------------------------|-----------------|-----------------|
| | μ _{10/400} | μ _{10/1000} | μ _{5/2000} | μ _{1/10000} | μ _{0.5/20000} | B ₈ | B ₂₅ | B ₅₀ |
| GT-100 | 20.4 | 16.2 | 9.6 | 2.8 | 1.2 | 1.82 | — | — |
| GT-050 | 16.6 | 16.0 | 9.9 | 2.7 | 1.5 | 1.75 | — | — |
| ST-150 | 9.61 | 8.17 | 5.57 | 1.70 | 1.15 | — | 1.56 | 1.66 |
| ST-100 | 8.54 | 7.87 | 5.81 | 2.00 | 1.39 | — | 1.55 | 1.65 |
| ST-050 | 3.13 | 3.11 | 2.65 | 1.00 | 0.93 | — | 1.47 | 1.58 |

- Notes) 1. For GT series, the specimens are taken from the strips parallel to the rolling direction. The measurements are in accordance with JIS C 2550 after stress relief annealing.
 2. For ST series, the specimens are taken from the strips in both directions of parallel and transverse to the rolling direction. The measurements are in accordance with JIS C 2550.

Table 8 Mechanical and electric properties

| Grade | Density (g/cm ³) | Space factor (%) | Tensile strength (N/mm ²) | Elongation (%) | Hardness (Hv) | Specific resistance (μΩcm) |
|--------|------------------------------|------------------|---------------------------------------|----------------|---------------|----------------------------|
| GT-100 | 7.65 | 93 | 420 | 9 | 202 *2 | 48 |
| GT-050 | 7.65 | 90 | 387 | 11 | 179 *3 | 48 |
| ST-150 | 7.65 | 94 | 496 | 15 | 205 *1 | 52 |
| ST-100 | 7.65 | 93 | 476 | 13 | 198 *2 | 52 |
| ST-050 | 7.65 | 90 | 487 | 12 | 182 *3 | 52 |

- Notes) 1. Tensile strength and elongation are measured parallel to the rolling direction.
 2. Hardness are measured by *1: H; 0.5kg, *2: H; 0.3kg, *3: H; 0.1kg.

Table 9 Comparison of properties between various magnetic materials

| Material | Magnetic flux density B ₈ (T) | DC max relative permeability μ _m | Core loss W _{1/20000} (W/kg) | Specific resistance (μΩm) |
|--------------------------------------|--|---|---------------------------------------|---------------------------|
| GT-100 | 1.82 | 24,000 | 35 | 0.48 |
| GT-080 ※ | 1.80 | 20,000 | 31 | 0.48 |
| GT-050 | 1.75 | 14,000 | 21 | 0.48 |
| GT-040 ※ | 1.70 | 10,000 | 18 | 0.48 |
| ST-150 | 1.44 | 10,000 | 55 | 0.52 |
| ST-100 | 1.42 | 7,000 | 44 | 0.52 |
| ST-050 | 1.26 | 2,500 | 26 | 0.52 |
| High silicon steel(0.1t) | 1.29 | 23,000 | 31 | 0.82 |
| Amorphous | 1.56 | 300,000 | 6 | 1.30 |
| Nanocrystalline soft magnetic alloys | 1.23 | 70,000 | 4 | 0.01 |
| Dust core(Sendust) | 0.65 | 150 | 62 | >10000 |
| Ferrite (Mn-Zn) | 0.45 | 3,500 | 3 | >100000 |

- Notes) Grade(※)shows newly developed products.

Oriented thin-gauge silicon steel strips GT-100

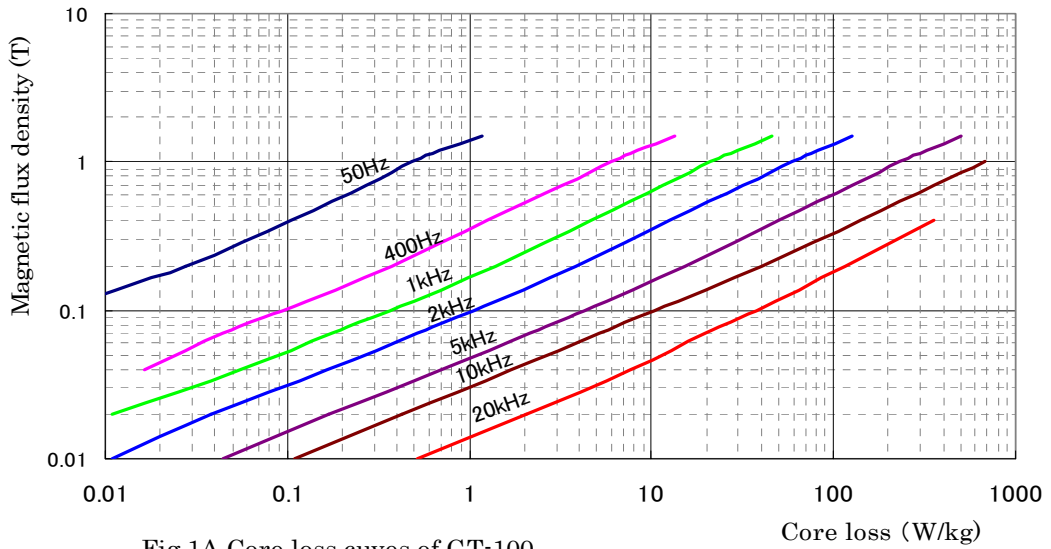


Fig.1A Core loss curves of GT-100

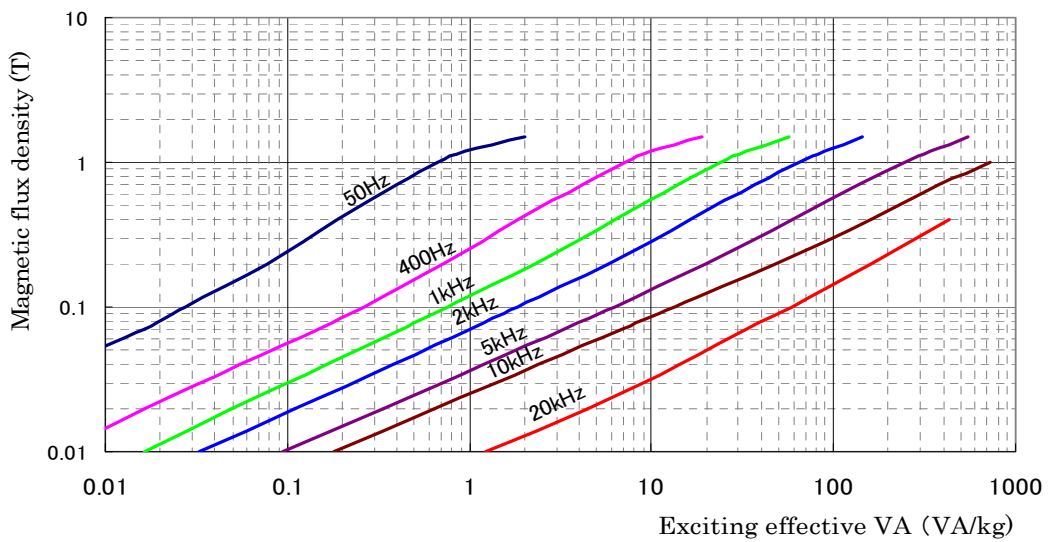


Fig.1B Exciting power curves of GT-100

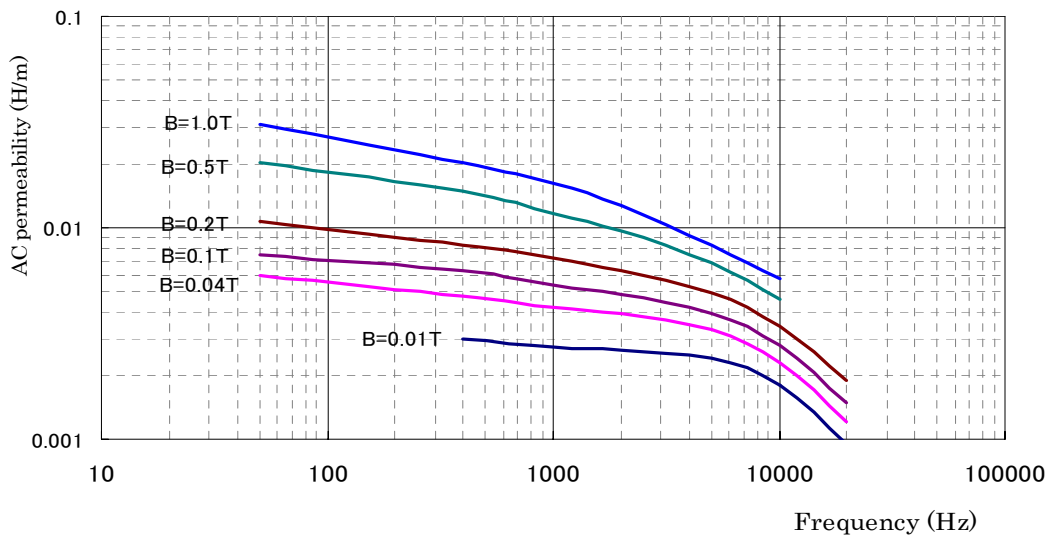
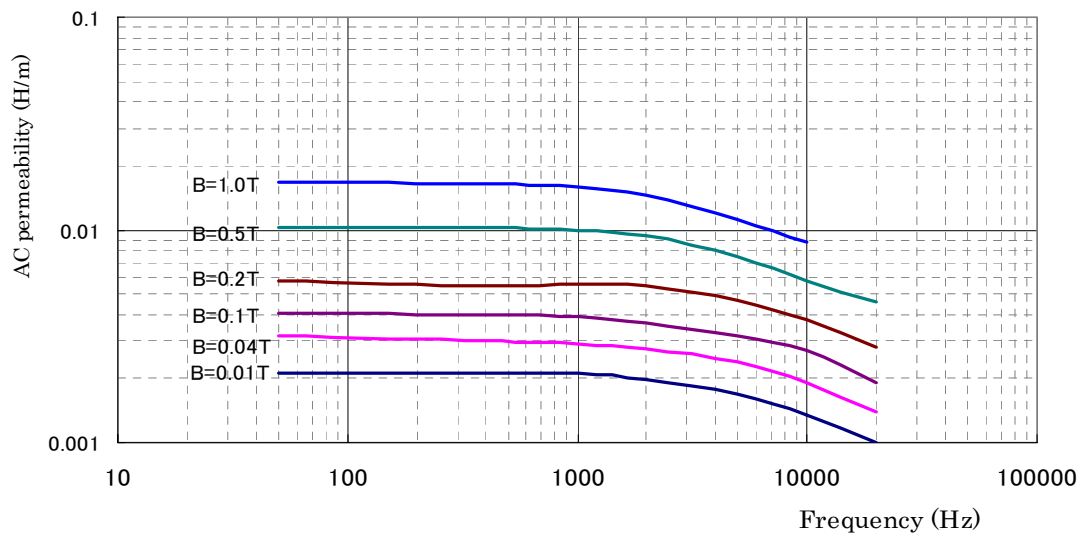
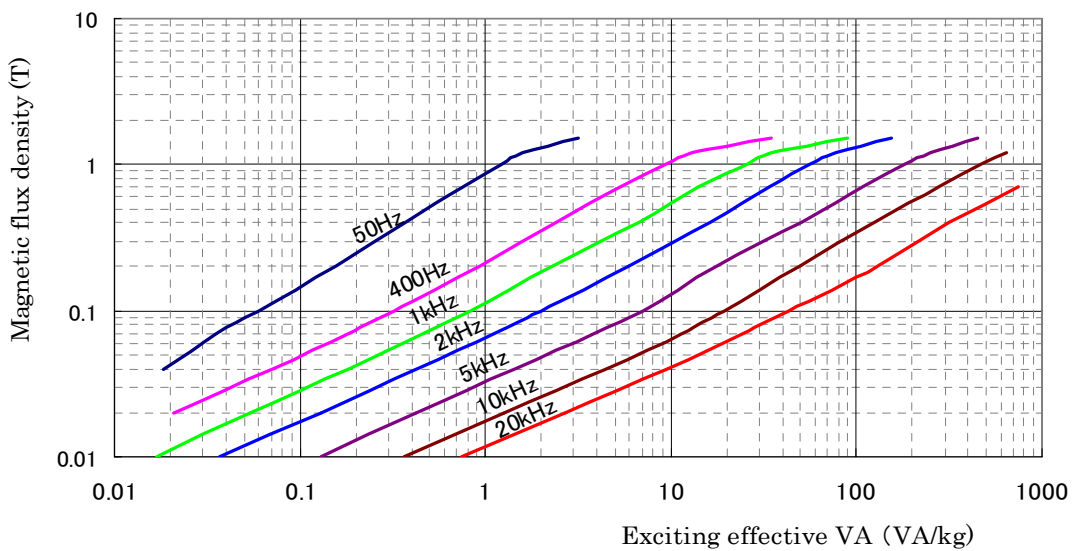
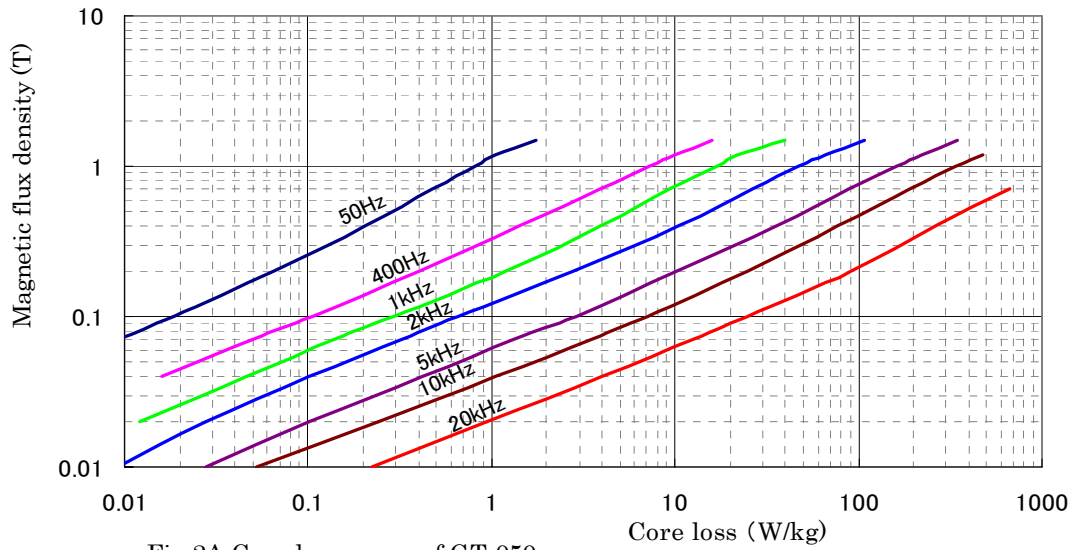


Fig.1C Frequency permeability characteristics curves of GT-100

Oriented thin-gauge silicon steel strips GT-050



Non-oriented thin-gauge silicon steel strips ST-150

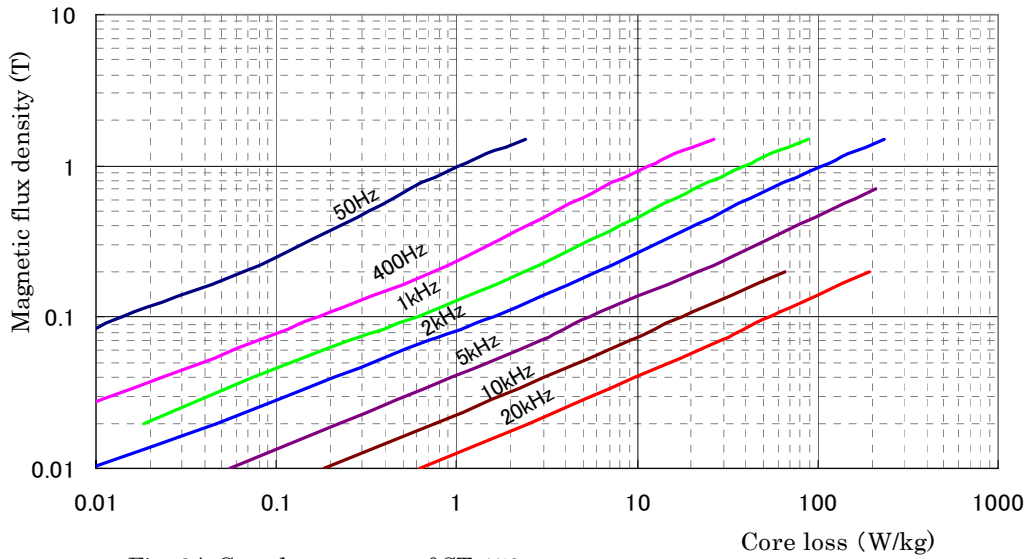


Fig. 3A Core loss curves of ST-150

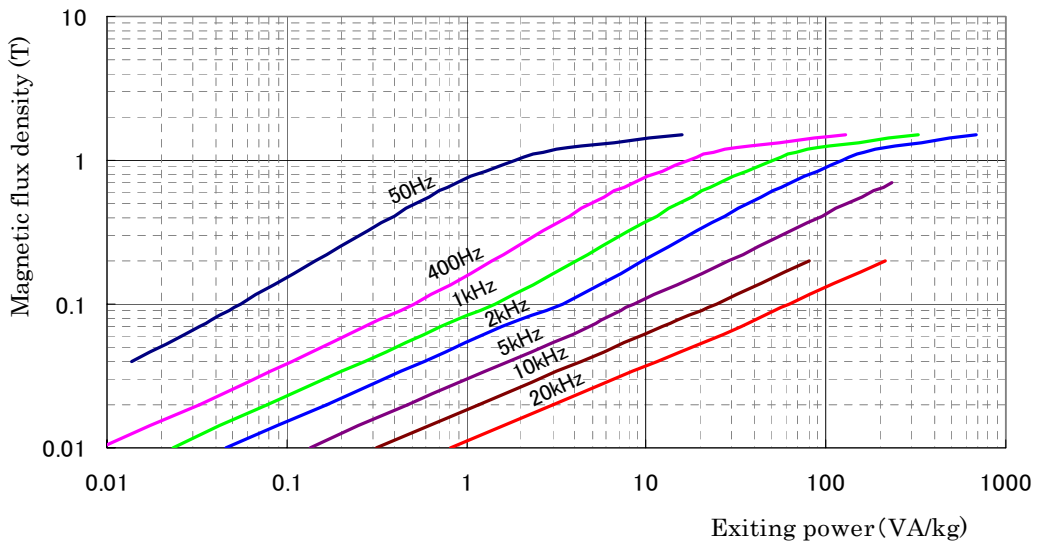


Fig.3B Exiting power curves of ST-150

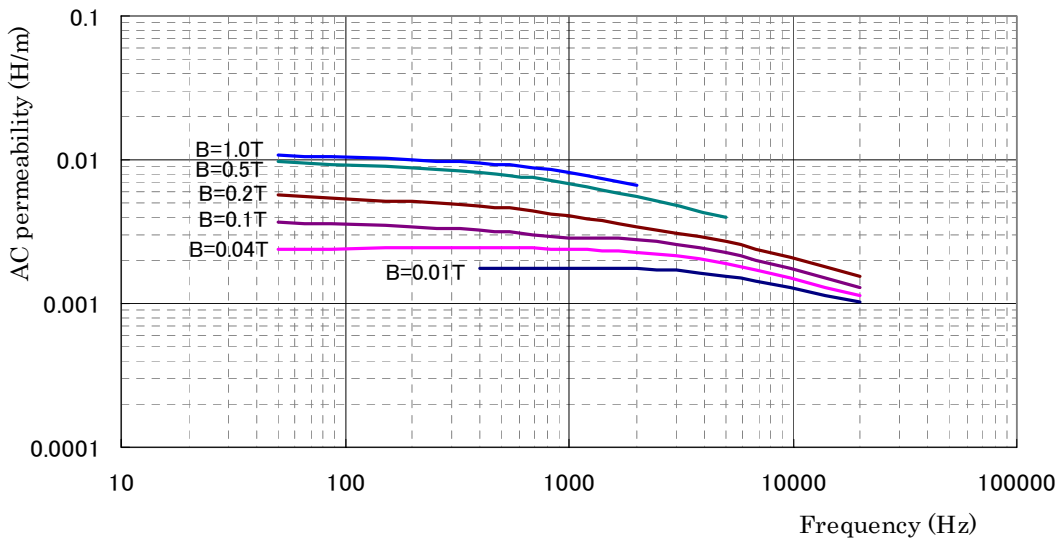


Fig.3C Frequency permeability characteristics curves of ST-150

Non-oriented thin-gauge silicon steel strips ST-100

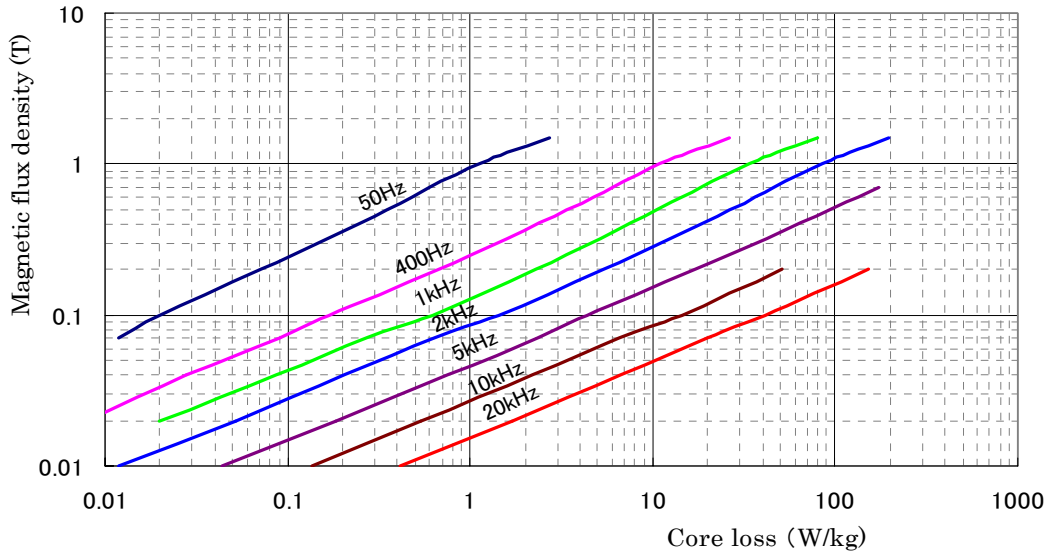


Fig. 4A Core loss curves of ST-100

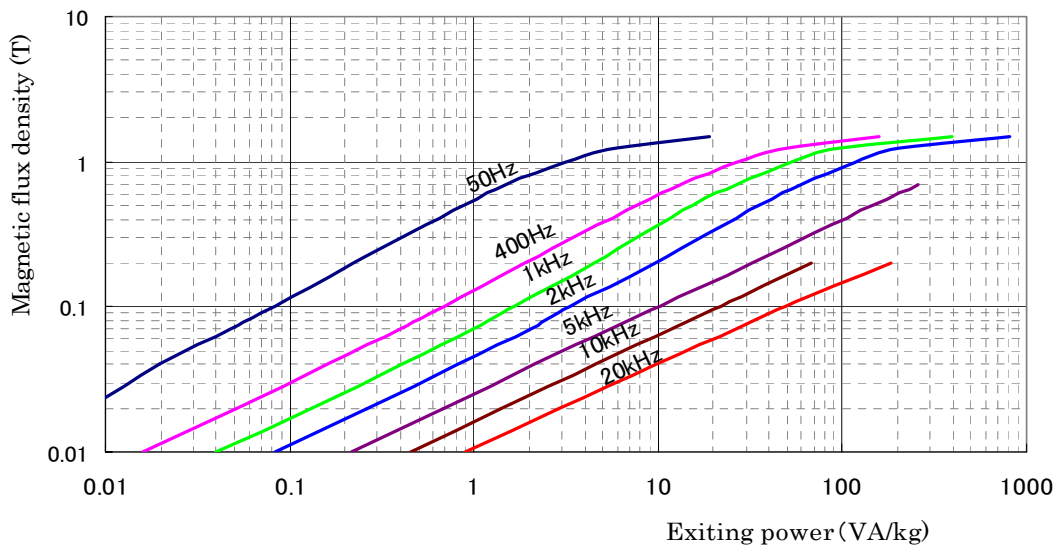


Fig.4B Exiting power curves of ST-100

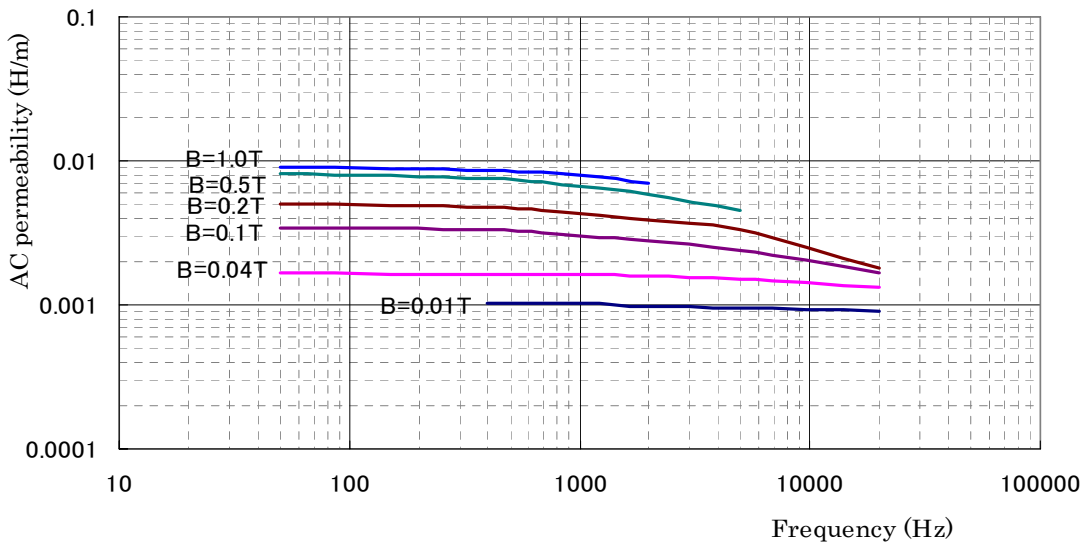


Fig.4C Frequency permeability characteristics curves of ST-100

Non-oriented thin-gauge silicon steel strips ST-050

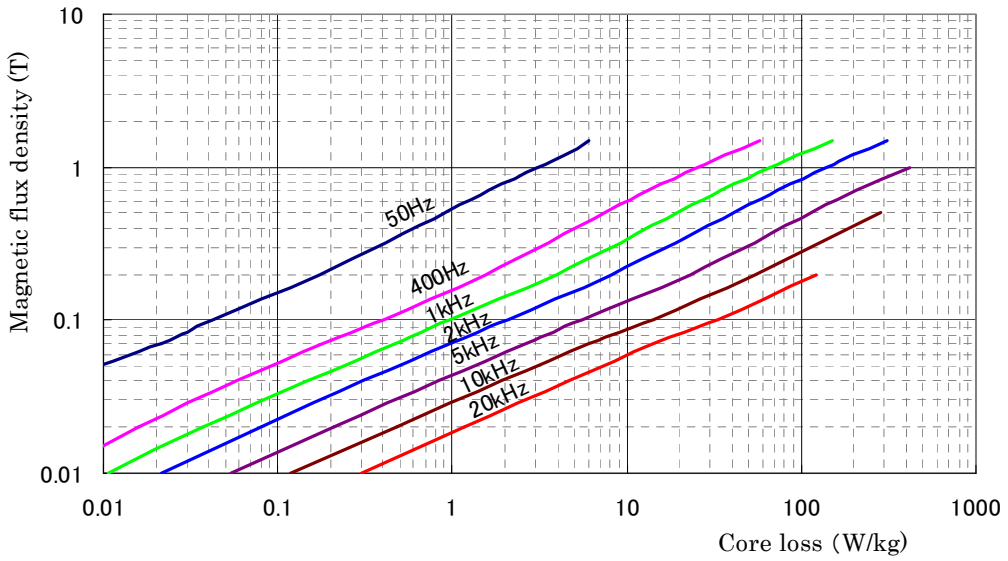


Fig. 5A Core loss curves of ST-050

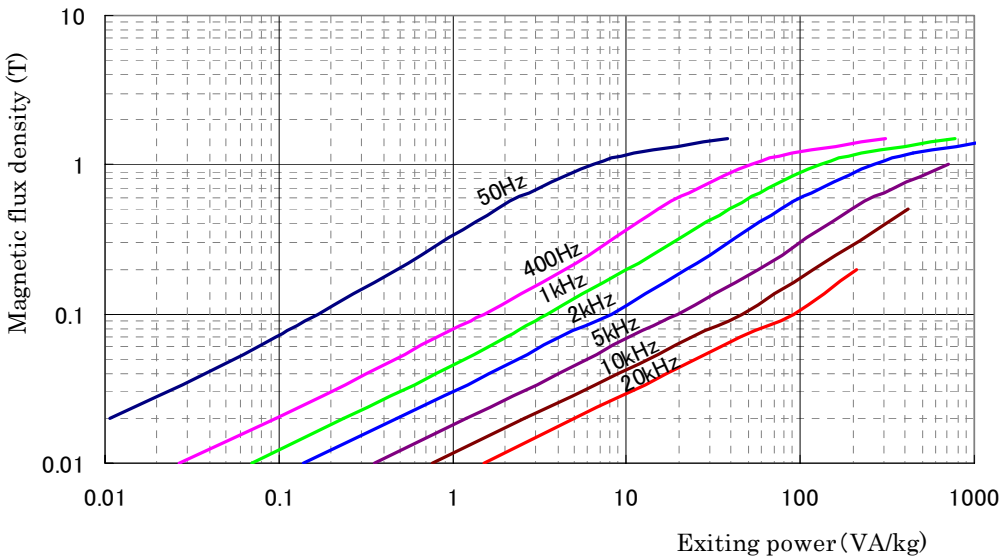


Fig.5B Exiting power curves of ST-050

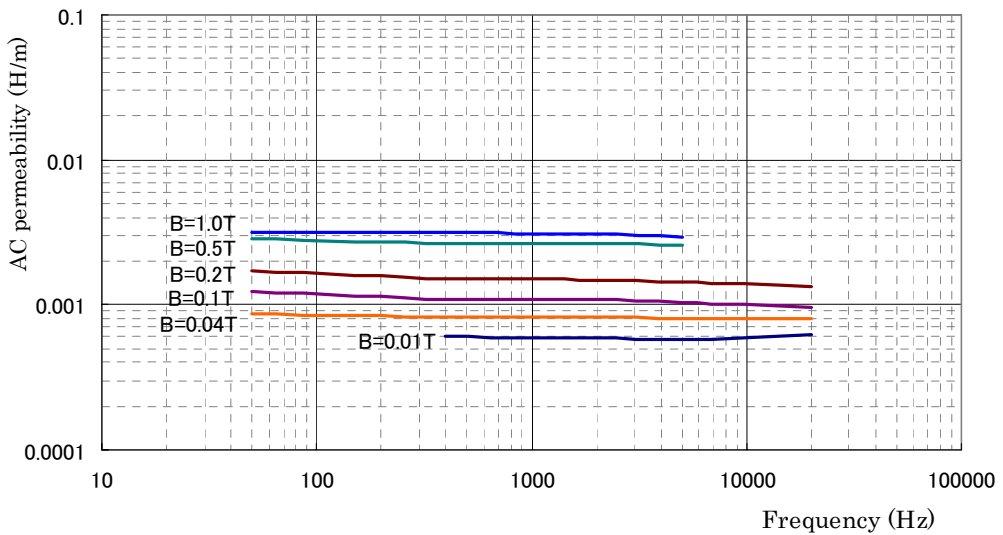


Fig.5C Frequency permeability characteristics curves of ST-050

The insulation coating

The insulation coating has the following characteristics.

1. The inorganic insulation coating is stable both thermally and chemically. Stress relief annealing is carried out in non oxidizing atmosphere at a temperature from 730 to 770°C, but the insulation coating has thermal resistance up to about 800°C. The coating is not damaged by transformer oil, and has high corrosion resistance.
2. The insulation coating is firmly adhered to the strip, so that it will not peel off during shearing and blanking.
3. The thin insulation coating allows high lamination factor.
4. The coating has high interlaminar resistance.

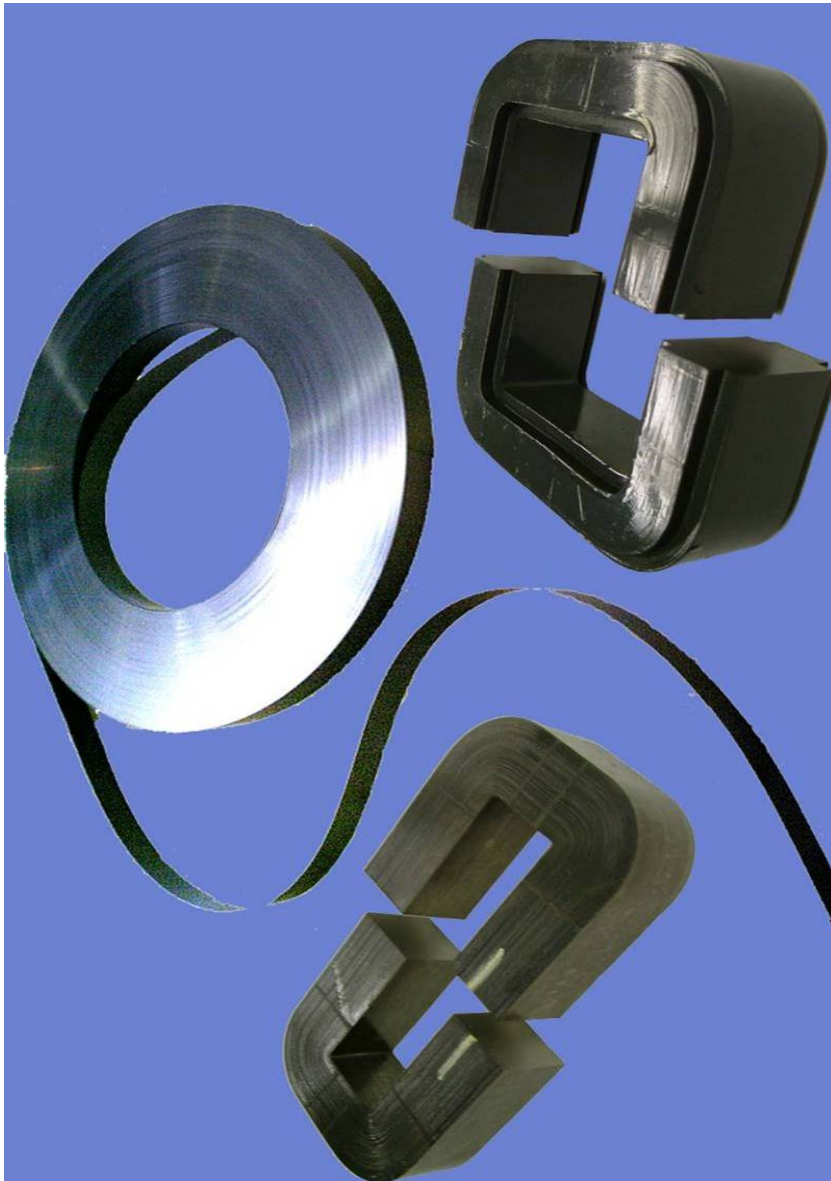
Stress relief annealing of wound cores

Stress from cutting, punching, bending have adverse effects on magnetic properties. To relieve these stress, stress relief annealing should be performed if necessary. The cautionary statements about stress relief annealing are as follows.

1. The atmosphere of stress relief annealing
Compositions of atmosphere gas are needed to be highly pure Nitrogen or mixed gas of 5-10% Hydrogen and 90-95% Nitrogen with the dew point less than 0°C.
2. Avoiding Carbon contamination
The thin-gauge silicon steel strips can be easily carburized by annealing, because they are low carbon steel. The spacer and the inner cover of batch-type furnace should be made from low carbon steel. Completely remove oil, paper and cloth.
3. Piling
Stacked cores should be heated in the edge to edge direction for a more efficient heat transfer for uniform heating. The heat radiation and the heat transfer by convection of atmosphere should be considered. Unlevel surfaces of the bases reduce the performance of the cores because of the induced strains.
4. Annealing temperature and time
Annealing temperature of 730~770°C, for 2~3 hours is recommended.
Cooling at the rate of 50~100°C/hr, the temperature of the furnace below 350°C when cores are removed will have the best results.

Substances of environmental concern

Our thin-gauge silicon steel strips are compatible in the RoHS directive that the mercury and its compounds, the cadmium and its compounds, the lead and its compounds, hexavalent chromium compounds, PBB and PBDE are below the restricted value and do not intentionally add or use in the manufacturing process.



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Notice

- (1) Excluding standard values, the technical data described in this catalogue does not guarantee values.
- (2) Products described in this catalogue may show properties different from described contents depending on the intended purposes and conditions of use. We will not be responsible for any damages.
- (3) Technical data in this catalogue is subject to change without previous announcements.
Please contact our sales department for the latest information.

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